

PATENT SPECIFICATION

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DRAWINGS ATTACHED.

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COMPLETE SPECIFICATION.

Improvements in Electrical Apparatus Having Foil Windings.

We, GENERAL ELECTRIC COMPANY, a Corporation organized and existing under the laws of the State of New York, United States of America, residing at 1, River Road, Schenectady 5, New York, United States of America, do hereby declare the invention for which we pray that a patent may be granted to us, and the method by which it is to be performed to be particularly described in and by the following statement:—

This invention relates to electrical apparatus, and more in particular to means for reducing current concentrations and resulting high temperature localizations in electrical foil windings.

In the past the use of foil windings for electrical induction apparatus, such as transformers and the like, has been limited to relatively low KVA applications because uneven current distribution in the foil windings has resulted in hot-spot temperatures that exceeded permissible values. Uneven current distribution in foil windings is caused by fringing of the magnetic leakage flux at the edges of the windings. The fringing of the flux lines at the edges of the winding causes the flux to cut across more of the foil sheets than at the central portion of the winding where the lines of flux are relatively straight. Consequently, a greater current density occurs at the edges of the winding because the induced current is closely related to the amount of flux that cuts across the conductor material from which the winding is made.

It has been found that the tendency of magnetic flux lines to fringe at the edges of an electrical foil winding can be reduced by subjecting the flux to a counter magnetomotive force that causes it to move in a straighter path. This reduces the amount

of flux which cuts across the winding edges and thus causes the relative current density at the edges of a foil winding to be closer to that at the interior portion of the winding. The resulting overall increase in uniformity of current density reduces the heat generated at the edges of the winding and allows such windings to be employed in higher KVA applications. Thus, by practicing the invention, foil windings can be employed in a larger number of instances in higher powered electrical induction apparatus.

The object of the invention is to provide means for shielding an electrical foil winding for reducing current concentrations in the electrical foil windings and eliminating the hot-spot temperatures.

According to the invention there is provided a shield structure for reducing current concentrations at the edge of a foil winding of an electrical apparatus, said structure comprising a substantially rectangular closed outer loop portion and an intermediate portion integral with said loop portion adjacent one end thereof and extending into said loop portion towards the opposite end thereof, said two opposed ends being separated by a narrow gap such that the structure is formed into a substantially cylindrical shape for enclosing the foil winding, the structure being formed of electrically conductive sheet material.

In the drawings:

Figure 1 is a perspective partially cross-sectional view of an embodiment of electrical apparatus in accord with the teachings of this invention.

Figure 2 is a cross-sectional partially broken away view taken along the lines 2—2 in Figure 1.

Figure 3 is a perspective view of an elec-

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trical shield in accord with the teachings of our invention

Fig. 4 is a cross-sectional view of a pair of windings and shields in accord with the teachings of our invention, with the magnetic flux acting on the winding schematically illustrated by arrows.

Fig. 5 is a perspective partially broken away view of an electrical winding and shield, showing a method of connecting the shield.

Referring now to the drawing, and more in particular in Fig. 1, an electrical transformer 10 in accord with this invention is schematically illustrated. The transformer 10 comprises a magnetic induction core 11 having yokes 15 and legs 12 which are surrounded by high voltage windings 13 and low voltage windings 14. The windings are made from continuous sheets of electrically conducting foil material, such as aluminum or copper foil, which are spirally wound around the respective core legs 12. According to a favored embodiment of this invention, the windings are provided with means, such as the shields 20, that produce a magnetomotive force which reduces fringing of the magnetic flux at the edges of the windings. From Fig. 2 it can be seen that the windings 13 and 14 may be disposed between two shields 20, one of which surrounds the core legs 12 and is itself surrounded by the winding 14, and the other shield surrounding the winding 13. It will be apparent from the description that follows that additional shield could be placed at other locations, as for example between the windings 13 and 14, without departing from the teachings of our invention.

A preferred embodiment of our shield structure is more clearly illustrated in Fig. 3. The shields 20 may be formed from substantially rectangular sheets of electrically conducting material which have been bent to a substantially cylindrical shape that enables them to surround the windings. The ends of the shields are separated by a narrow gap 28 that prevents them from becoming short-circuited turns. Each shield 20 comprises a closed outer peripheral loop 31 of conducting material which defines an open central portion 22. The peripheral loop 31 may comprise a first edge portion 23, a second edge portion 24, and end portions 25. It is thus apparent that if the shield 20 were laid out as a developed surface, the portions 23, 24, and 25 would define a closed substantially rectangular peripheral loop at its edges. An intermediate portion 26 of the shield is connected to the peripheral edge or loop 31 and extends into the open portion 22. It should be noted that the second edge portion 24 is wider in its axial dimension than the intermediate portion 26, which in turn is wider than the

first edge portion 23. The reason for this will be given in a paragraph that follows.

The windings 13 and 14 and the shields 20 may be supported by blocks of insulating material 30 of Fig. 1 in the conventional manner. Also the shields 20 at the upper end of the windings may be supported on the shields at the lower end of the windings by spacer blocks 31 of insulating material. The shields and high and low voltage windings of the transformer 10 may be separated by conventional spacers of insulating material (not illustrated) to provide passages for flow of an insulating and cooling fluid.

Referring now to Fig. 4, the effect produced by the shields 20 is illustrated by the arrows 40, 40', and 41, which schematically indicate the flux of the magnetic field passing through the winding and shields. The arrows 40 and 40' represent the main leakage flux produced by the load current in the windings 13 and 14. The dotted arrows 41 represent the flux caused by the current induced in the shields 20. It should be noted that the flux 40 is relatively straight at the central portion of the windings 13 and 14, but tends to fringe radially outwardly and inwardly at the end of the windings. Consequently, more flux lines cut across the layers of the conducting foil material at the ends of the windings and thus produce a higher concentration of current at the ends of the windings than at the center portion thereof. If the lines of flux were perfectly straight and parallel to the axial sides of the layers of foil conductor material from which the windings are made, the distribution of current through the winding would be uniform. Thus, any phenomenon which tends to straighten the path travelled by the lines of flux to approach this condition tends to make the distribution of current in the winding more uniform. The shields 20 are in the magnetic field of this leakage flux, and are thus linked by the lines of flux. Consequently, a current is induced in each shield 20, and this current itself produces a magnetic field represented by the arrows 41. The shield produced flux 41 is counter to the radial component of the flux 40 and thus tends to straighten the path travelled by the flux 40 to cause it to flow in a more nearly axial path. This reduces the fringing of the flux 40 at the ends of the winding and thus produces a more uniform concentration of current in the winding. Also, some of the flux 40 will try to escape the confining effect of the shields 20, and consequently some of the lines of flux 40' tend to fringe radially outwardly between the shields 20 and thus cut across more conductor foil layers near the central portion of the windings and induce more of a current in that portion. This also tends to increase the concentration of

current near the central portion of the windings and thus makes the overall current distribution more uniform.

It has been found by experimentation that 5 a triple element shield, in accord with the preferred embodiment of our invention, produces better results than a shield made from a whole piece of metal of roughly the same dimensions. The explanation for this is 10 believed to be that in a whole metal shield the concentration of flux produced in the shield by the induced current is spread over a large area and thus cannot be concentrated 15 opposite the edge of the winding where it will have the greatest effect. On the other hand, in our preferred shield embodiment, the intermediate portion 26 is located directly opposite the edge of the winding with the edge of the portion 26 being substantially level with the terminal edge of 20 the winding, and has a relatively high current concentration therein. This increases the density of the counter flux 41 at the edge of the winding because the flux density 25 is proportional to current density. It has also been found by experimentation that a triple element shield having its intermediate portion 26 connected at one end only so as to form a gap 27 at the unconnected end 30 produces the best results.

The first edge portion 23 of the shield is relatively small in axial height in order that the length of the core leg, commonly called the window height, can be kept to 35 a minimum. The second edge portion 24 of the shield 20 may be made as long as possible in the axial direction in order to increase the amount of current induced in the shield and thus the strength of the counter field it produces. This dimension is empirically arrived at and can be determined by trying various lengths until a point of diminishing returns is reached. The intermediate portion 26 of the shield is made 40 to an axial dimension that will concentrate the flux at the edge of the shield where it will produce the most useful result. The extent of this axial dimension is also empirically arrived at, but is generally a dimension 45 intermediate that of the first and second portions 23 and 24.

In Fig. 5 the shield 20 is shown to be 50 electrically connected to a lead 30 which is connected to the outer turn of a high voltage winding 13. This causes the shield 20 to be at the same electrical potential as the winding, and thus the shield reduces the 55 electrical stresses on the insulation of the winding by reducing the voltage gradient at the edge of the coil. Thus when shields are 60 also employed as the means for reducing the fringing of flux, the shields can be used to serve two functions.

It will be apparent to those skilled in the 65 art that it is virtually impossible to measure

the current distribution in a foil winding by direct methods. Consequently, an electrolytic analog tank was constructed so as to be analogous to foil windings with no shield. Tests were run to determine the 70 distribution of current in such windings. The tank was then modified so as to be analogous to foil windings shielded by a shield having the structure illustrated in the drawing. Tests were run on this tank analog, and the results showed marked improvement in current distribution as a result of the addition of shields. Temperature distribution tests were run on actual foil wound 75 transformers, and these tests showed that a reduction in hot spot temperatures at the edge of the windings occurred as a result of the addition of a flux confining shield in accord with the teachings of this invention.

It has been shown that by subjecting a 80 magnetic field that fringes at the edges of an electrical foil winding to a counter magnetic field, the current distribution in the winding can be improved, with a resulting lowering of hot spot temperatures. It will 85 be appreciated by those skilled in the art that means other than the specific shield illustrated in the drawing could be employed to achieve this desirable result. For example, shield means with an alternating current 90 directly applied to the shield, instead of a flux induced current, could be employed to produce a counter-magnetic field. Thus, a broader aspect of our invention is the method of obtaining a more uniform current 95 distribution in an electrical foil winding by opposing the tendency of magnetic flux to fringe at the edges of the winding by subjecting the flux to a counter electrical force.

It will be understood, of course, that while 100 the forms of the invention herein shown and described constitute preferred embodiments of the invention, it is not intended herein to illustrate all of the equivalent forms or ramifications thereof. It will also be understood that various changes may be made 105 without departing from the scope of the invention herein claimed.

WHAT WE CLAIM IS:—

1. A shield structure for reducing current concentrations at the edge of a foil winding of an electrical apparatus, said structure comprising a substantially rectangular closed outer loop portion and an intermediate portion integral with said loop 110 portion adjacent one end thereof and extending into said loop portion towards the opposite end thereof, said two opposed ends being separated by a narrow gap such that the structure is formed into a substantially 115 cylindrical shape for enclosing the foil winding, the structure being formed of electrically conductive sheet material.

2. A structure according to claim 1

wherein means are provided for electrically connecting the shield structure to the foil winding.

3. A shield structure for reducing current concentrations at the edge of a foil winding of an electrical apparatus, said structure substantially as described with reference to the accompanying drawings.

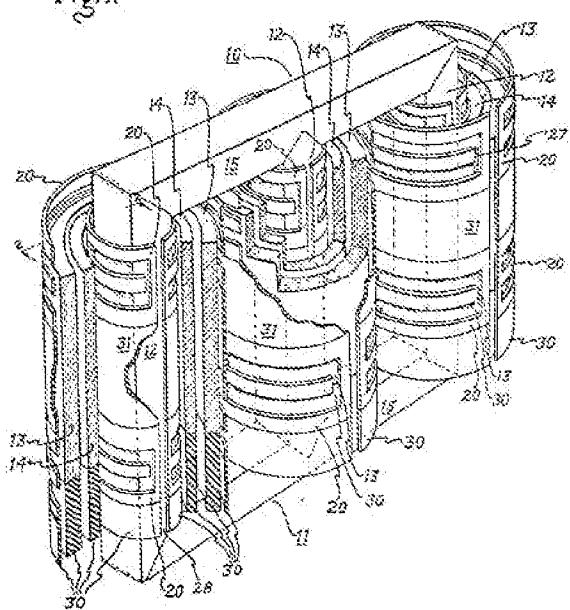
4. An electrical apparatus including a

shield structure according to any one of claims 1 to 3.

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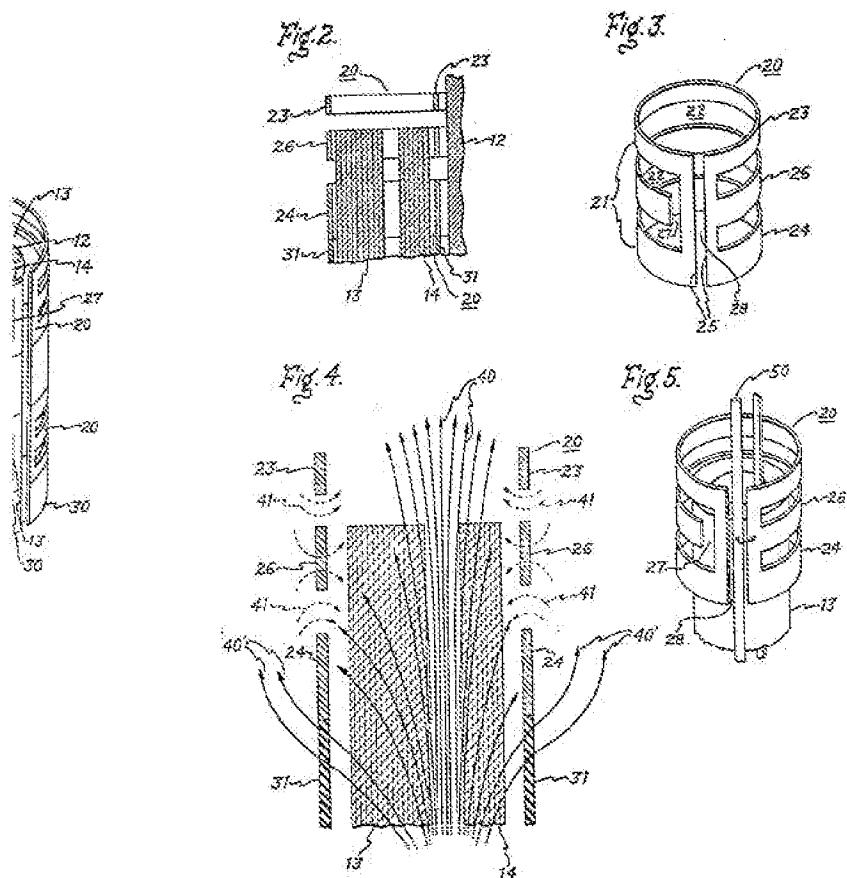
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Fig. 1.



990418 COMPLETE SPECIFICATION

2 SHEETS This drawing is a reproduction of
the Original on a reduced scale
Sheets 1 & 2



958415 COMPLETE SPECIFICATION
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